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# The spectrum of a 1- $\mu$ m-wavelength-driven tin microdroplet laser-produced plasma source in the 5.5–265.5 nm wavelength range

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Z. Bouza,<sup>1</sup> D J. Byers,<sup>2</sup> D J. Scheers,<sup>1,3</sup> R. Schupp,<sup>1</sup> Y. Mostafa,<sup>1</sup> L. Behnke,<sup>1</sup> Z. Mazzotta,<sup>1</sup> J. Sheil,<sup>1</sup> W. Ubachs,<sup>1,3</sup> R. Hoekstra,<sup>1,4</sup> M. Bayraktar,<sup>2</sup> A. Bayraktar,<sup>2</sup> R. Hoekstra,<sup>1,4</sup> K. Bayraktar,<sup>2</sup> A. Schupp,<sup>1</sup> K. K. K. Schupp,<sup>1</sup> K. K. Schupp,<sup>1</sup> K. K. Schupp,<sup>1</sup> K. K. Schupp,<sup>1</sup> Schupp,<sup>1</sup> K. Schupp,<sup>1</sup> K. Schupp,<sup>1</sup> Schupp,<sup>1</sup> Schupp,<sup>1</sup> K. Schupp,<sup>1</sup> K. Schupp,<sup>1</sup> Schupp,<sup>1</sup> K. Schupp,<sup>1</sup> Schupp,<sup>1</sup> K. Schupp,<sup>1</sup> Schupp,<sup>1</sup> K. Schupp,<sup>1</sup> K. Schupp,<sup>1</sup> Schupp,<sup>1</sup> K. Schupp,<sup>1</sup> K. Schupp,<sup>1</sup> K. Schupp,<sup>1</sup> Schupp,<sup>1</sup> K. Schup,<sup>1</sup> K. Schup,<sup>1</sup>

# **AFFILIATIONS**

<sup>1</sup>Advanced Research Center for Nanolithography, Science Park 106, 1098 XG Amsterdam, The Netherlands

<sup>2</sup>Industrial Focus Group XUV Optics, MESA+ Institute for Nanotechnology, University of Twente,

Drienerlolaan 5, 7522 NB Enschede, The Netherlands

<sup>3</sup>Department of Physics and Astronomy, and LaserLaB, Vrije Universiteit, De Boelelaan 1081, 1081 HV Amsterdam, The Netherlands

<sup>4</sup>Zernike Institute for Advanced Materials, University of Groningen, Nijenborgh 4, 9747 AG Groningen, The Netherlands

<sup>a)</sup>Author to whom correspondence should be addressed: versolato@arcnl.nl

#### ABSTRACT

We present a calibrated spectrum in the 5.5–265.5 nm range from a microdroplet-tin Nd:YAG-laser-produced plasma under conditions relevant for the production of extreme ultraviolet (EUV) light at 13.5 nm for nanolithography. The plasma emission spectrum obtained using a custom-built transmission grating spectrometer results from a careful calibration of a series of filters enabling measurements free of any higher diffraction orders. Specifically, Zr, Si, and Al thin-foil filters and bulk LiF, MgF<sub>2</sub>, and UV fused silica filters are employed. A further filter using four SiC mirrors is used to record the otherwise inaccessible 40–100 nm range. The resulting corrected and concatenated spectra are shown to accurately match in their respective overlap regions. The possibility to measure spectra over this broad range enables the optimization of current and future sources of EUV light for nanolithography by providing the diagnostics required for minimizing the emission of unwanted wavelength bands.

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# I. INTRODUCTION

Laser-produced plasma (LPP) generated from liquid tin (Sn) microdroplets provides extreme ultraviolet (EUV) light for modern nanolithography,<sup>1–7</sup> enabling the continued reduction of feature sizes on affordable integrated circuits (ICs). Such laser-produced plasmas of tin are characterized by a strong emission peak near 13.5 nm, originating from transitions between complex excited states in multiply charged Sn<sup>10+</sup>–Sn<sup>15+</sup> ions.<sup>8–17</sup>

Multilayer optics are used in industrial lithography machines to collect the EUV light from its source and to provide an image of the so-called mask onto the wafer. These optics are designed to reflect wavelengths in a 2%-wavelength bandwidth centered around 13.5 nm (the bandwidth limitation is, in part, due to the many ~10 required reflective surfaces).<sup>18,19</sup> As such, most spectroscopic works

on Sn LPPs have focused on the "in-band" wavelength region<sup>17,20-24</sup> or on nearby out-of-band (OOB) EUV emission features, <sup>14,23,25-31</sup> spectral regions of which may help diagnose the plasma in terms of its main in-band emitters' charge states or temperature. Little spectroscopic information is available for longer vacuum (VUV)- and deep-ultraviolet (DUV) wavelengths, in particular, in terms of relative (or absolute) emission intensities. Available spectra in the literature show either vacuum- or deep-ultraviolet spectra without the EUV region around 13.5 nm,<sup>32–36</sup> or if the EUV region is presented, the spectral range between EUV and DUV is not shown.<sup>37–42</sup>

VUV/DUV emission may be transported through the multilayer optics systems and expose the wafer. Given the significant photon energy, this exposure may influence the chemical processes on the wafer and negatively impact imaging contrast and quality.<sup>43,44</sup> As such, it is of significant interest to understand in detail the spectrum of EUV generating LPPs in terms of their absolute emission intensity. This will enable identifying the origins of many yet-unknown emission features and enable the development of mitigation strategies, i.e., minimize the OOB emission. In particular, the wavelength range of 30–90 nm is important for EUV lithography due to the strong absorption by hydrogen, which is present as a buffer gas in the EUV source chambers. Photoionization of hydrogen molecules by DUV radiation generates plasmas in the scanner that can degrade important optical components.<sup>45</sup> It is challenging to obtain the source spectrum in this wavelength range due to strong contributions from higher diffraction orders of the very strong emission feature centered around 13.5 nm.

We present an intensity-calibrated spectrum of a droplet-based tin plasma driven by 1- $\mu$ m laser light in the wavelength range between 5.5 and 265.5 nm. A custom-built transmission grating spectrometer (TGS) is used to record the spectrum using a 1000 lines per mm grating. Higher diffraction orders, which would otherwise render impossible the detection of longer wavelengths, are eliminated by using Zr, Si, Al, LiF, MgF<sub>2</sub>, and UV fused silica (UVFS) filters. An additional novel filter using four SiC mirrors is used to record the 40–100 nm region, which would, given the dominant contribution from the higher diffraction orders of the EUV band if unfiltered, otherwise remain inaccessible. Careful calibration of these filters and the transmission grating combined with the response of the camera enables the absolute calibration of the full operating band and obtaining a spectrum free of any higher diffraction orders.

# **II. EXPERIMENTAL SETUP**

In our experiments, molten tin microdroplets of 46  $\mu$ m diameter are first irradiated by a relatively low intensity (~10<sup>9</sup> W/cm<sup>2</sup>), 1- $\mu$ m-wavelength pre-pulse (PP) from an Nd:YAG laser.<sup>46</sup> The microdroplets are dispensed from a droplet generator inside a vacuum vessel with a background pressure of ~10<sup>-6</sup> mbar. The beam profile of the PP laser is Gaussian with a spatial full width at half maximum (FWHM) of 97  $\mu$ m. The temporal profile is a Gaussian with a FWHM of 29 ns. For the presented experiments, a constant PP energy of 6.8 mJ was used. The PP deforms the droplets into thin sheet targets, which are radially symmetric and thickest in their center.<sup>47-51</sup> The target diameter is controlled via a time delay between the pre- and main pulses (MPs), and for our experiments, the time delay is set to 2000 ns, leading to a target diameter of ~320  $\mu$ m.

After the PP, the targets are irradiated with a high-intensity 1- $\mu$ m-wavelength main pulse (MP) from a Nd:YAG laser. The pulse duration of the MP is 10 ns, and the focal spot has a Gaussian beam profile with a FWHM of 103  $\mu$ m. For the presented experiments, a fixed laser intensity of 2.3 × 10<sup>11</sup> W/cm<sup>2</sup> was employed using a pulse energy of 293 mJ. The intensity was calculated as described in Ref. 27. Additional details regarding the droplet-based experimental setup can be found in Ref. 47. Finally, a simplified scheme of the experimental setup is presented in Fig. 1.

The spectral emission from the Sn laser-produced plasma is recorded using a broadband transmission grating spectrometer<sup>52,53</sup> placed under an angle of 60° with respect to the incoming laser light. The different elements in the TGS are shown schematically in Fig. 1. The spectrometer is operated with a slit width of 50  $\mu$ m and a 1000 lines/mm transmission grating, achieving a FWHM instrument

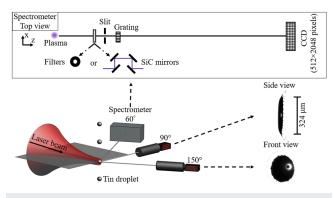


FIG. 1. Experimental setup showing the front- and side-view shadowgraphs of the tin targets used for plasma generation as recorded by two cameras. The upper boxed figure is a schematic of the transmission grating spectrometer.

resolution of 0.8 nm at 13.5 nm.<sup>52</sup> The use of the 1000 lines/mm transmission grating allows one to record emission in the 5.5-265.5 nm-wavelength region. The limits to this specific 5.5-265.5 nm range are set on the short wavelength side by the onset (>5.5 nm) of the availability of calibration data for the diffraction grating (see Sec. III B). On the long wavelength side, the limit (<265.5 nm) is due to the geometry of the spectrometer. Furthermore, the spectrometer contains Zr, Si, Al, LiF, MgF<sub>2</sub>, and UVFS filters and SiC mirrors as tabulated in Table I. The Zr, Si, and Al filters are foil filters with a common thickness of 200 nm. The foils are supported with a Ni mesh with 10 lines/in. period. The SiC system comprises four bulk-SiC mirrors placed under an angle of 45° with respect to the optical axis (see Fig. 1). The transmission grating, the Zr, Si, and Al filters, and the SiC mirrors are calibrated at the beamline facilities of the Physikalisch-Technische Bundesanstalt (PTB), at the BESSY-II synchrotron, Berlin, limited to wavelengths >5.5 nm. The LiF, MgF<sub>2</sub> and UVFS filters are calibrated for wavelengths down to 115 nm using a vacuum-ultraviolet spectrograph equipped with a deuterium lamp.

The diffracted light in the TGS is recorded on a backilluminated charge-coupled device (CCD) from greateyes GmbH (GE2048 512BI UV1). The CCD is cooled to -30 °C to reduce thermal noise. Background images are then subtracted from the recorded spectra to eliminate the dark counts and read-out noise. The resulting CCD images are cropped and corrected for shear and

**TABLE I.** Filters used in the spectral measurements with the transmission grating spectrometer. All short wavelength cutoffs are specified at 50% of the maximum transmission shown in Figs. 2–4.

Filter material	Filter type	Thickness	Short wavelength cutoff (nm)
Zr	Foil	200 nm	6.1
Si	Foil	200 nm	12.5
Al	Foil	200 nm	17
SiC	Mirrors	1 mm	55
LiF	Window	2 mm	129
MgF <sub>2</sub>	Window	2 mm	<115 <sup>a</sup>
UVFS	Window	2 mm	165

 $^{\rm a}{\rm At}$  115 nm, the transmission is  $~\sim\!53\%$  of the maximum.

tilt that may be introduced by a misalignment of the slit and the grating with respect to the CCD pixel array. Next, the pixel counts are averaged along the non-dispersive axis and corrected for the respective exposure times. The resulting spectra are then corrected for filter efficiency, the first-order diffraction efficiency of the grating, the camera response, and the solid angle of the spectrometer. The spectrometer has a solid angle of  $37 \times 10^{-11}$  sr that is calculated using the slit width, pixel size, and distance to the plasma.

For the wavelength calibration, a measurement with the Al filter is used. The sharp filter edge at 17.056 nm<sup>54</sup> and its higher orders enable accurate calibration of the wavelength axis. Here, the higher diffraction orders are advantageous for wavelength calibration.

# **III. RESULTS**

In this section, three necessary types of corrections are applied to the raw spectra, namely, the (A) filter transmission, (B) grating diffraction efficiency, and (C) CCD response.

## A. Filter transmission

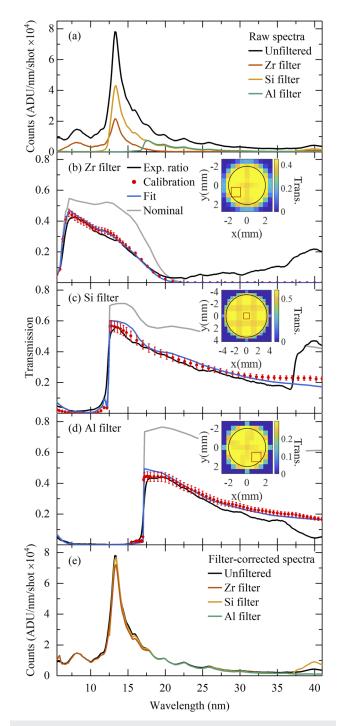
Spectra were recorded in the 5.5–265.5 nm-wavelength region using different filters. The advantage of capturing spectra using different filters is that each filter allows for the measurement of different wavelength regions clear from higher-order contributions. In the following, we sub-divide our discussion of the 5.5–265.5 nm spectra into three regions: (1) 5.5–40 nm, (2) 40–115 nm, and (3) 115–265.5 nm, and we discuss each region individually.

#### 1. 5.5-40 nm wavelength range

For the investigation of the 5.5-40 nm wavelength range, we recorded four sets of spectra using (i) no filter and the filters (ii) Zr, (iii) Si, and (iv) Al. The measured spectra are presented in Fig. 2(a).

The Zr filter has a cutoff at ~6.1 nm that allows for recording a higher-order-free tin LPP spectrum in the ~6.1 to 12.2 nm region. The Si filter exhibits a cutoff at ~12.5 nm, so in that way, the spectrum is pure in the range of ~12.5 to 25 nm. The Al filter has the advantage of a longer wavelength cutoff at ~17 nm such that all orders of the strong 13.5 nm emission feature are absent and a clean measurement in the range ~17 to 34 nm is possible.

The transmission functions of the various filters are tabulated in the CXRO database;<sup>54</sup> however, such transmission data are only valid for pristine samples. These filters typically suffer from oxidation and are subject to contamination from hydrocarbons and tin deposition. To obtain reliable transmission functions, the filters are calibrated at the PTB in Berlin. The calibration results are shown in Figs. 2(b)-2(d). The calibration procedure comprises two steps. First, for each filter type, the entire filter area was sampled at a single wavelength (13.5 nm for the Al filter and 17.5 nm for the Si and Zr filters) using a  $0.5 \times 0.5 \text{ mm}^2$  beam, enabling one to obtain a detailed "map" of the transmission. Second, at one particular position on the filter (indicated by red squares in the inset figures), the full wavelength range is measured. The recorded transmission function was subsequently scaled by a factor proportional to the average transmission at the wavelength of the first measurement step (within the filter window indicated by the black circle in the inset figures). The error bars on this scaled transmission curve [red data points in Figs. 2(b)-2(d)] represent one standard deviation from the average across the filter.



**FIG. 2.** (a) Raw emission spectra obtained from tin LPP using Zr, Si, and Al filters, and using no filter. ADU: arithmetic digital unit. Filter transmissions for (b) Zr, (c) Si, and (d) Al filters. The experimental ratio is the result of the division of the respective filtered by the unfiltered spectra, the calibration is from PTB, and the fitted curve is obtained taking oxidation into account, while the nominal one is the transmission obtained CXRO. Insets: transmission maps measured at 13.5 nm for Zr and Si and at 17.5 nm for Al. Red squares depict the location of the filter used for the wavelength scan. (e) Spectra corrected for the respective filter transmission functions.

Superimposed in black in the same figures are experimental estimates of the transmission function. These estimates are obtained by dividing the respective filtered spectra by the unfiltered spectra. These ratios may serve only as estimates as they are influenced by higher diffraction orders.

In all cases, the filter transmission is significantly lower than theoretical transmission that would be obtained from the CXRO database using the nominal thickness (shown as light gray lines). In an attempt to quantitatively explain the differences between the calibration and nominal CXRO database entries, we simulate the influence of finite oxidation of the filter surfaces using the following equation (Al as an example):

$$\Gamma = \exp(-n_{\mathrm{Al}}\mu_{\mathrm{Al}}d_{\mathrm{Al}}) \times \exp(-n_{\mathrm{Al}_2\mathrm{O}_3}\mu_{\mathrm{Al}_2\mathrm{O}_3}d_{\mathrm{Al}_2\mathrm{O}_3}).$$
(1)

The symbols n,  $\mu$ , and d represent the number of atoms per unit volume, atomic photo-absorption cross section, and thickness of the material, respectively. Thin film interference effects are verified to be negligible. We also accounted for the thickness of the non-oxidized part of the filter, and the fraction of the filter material in the oxide layer sums up to the nominal thickness. The fraction of the filter material in the oxide layer is calculated by considering the atomic weights of the pure filter material and the oxidized filter material. For Al, this fraction is calculated as  $W_{Al_2O_3}$ , where W is the atomic/molecular weight. This consideration allows fitting the  $T(\lambda)$ function to the PTB measured transmission curve with a single free fit parameter, namely, the thickness of the oxide layer. The fit results shown in Fig. 2 are in good agreement with the calibration data. The obtained oxide thicknesses range from 17 nm in the Al filter case to 49 nm in the Zr filter case. We find optimum agreement between the simulated and experimentally determined calibration curves for the oxide layer thickness of 49 nm ZrO<sub>2</sub> layer (with 169 nm pure Zr remaining), 19 nm SiO<sub>2</sub> (192 nm pure Si), and 17 nm Al<sub>2</sub>O<sub>3</sub> (193 nm pure Al). The substantial oxide layers (we assume that the oxide layer is divided between front and back sides of the filter) are, in fact, in agreement with the expected oxide layer thickness of such metal foils. More specifically, it has been shown in Ref. 55 using Auger depth profiling that a 100 nm thick Zr filter can have 10 nm thick oxide layers on both sides of the filter. The total oxide layer thickness in Ref. 55 is of the same order of magnitude as the oxide layer thickness we have found. The same study<sup>55</sup> further shows that carbon and carbide mixed with Zr are also present throughout the filter, decreasing the transmission further. Since carbon and carbide mixing is not taken into account in our analysis, our calculations may overestimate the ZrO<sub>2</sub> layer thickness. For the Si filter, a total oxide layer thickness of 66 nm has been reported, somewhat thicker than what we found.<sup>56</sup> For the Al filter, oxide thicknesses around 15 nm have been reported, which match well with the 17 nm thickness that is found here.<sup>56,57</sup> All in all, the PTB-calibrated transmission curves can be well understood from our model assuming a relatively thick oxide layer coating the pure filter surfaces.

Next, the spectra are corrected with the filter transmission data from PTB, the results of which are shown in Fig. 2(e). The corrected spectra are shown starting from the short wavelength cutoff of each filter onward until the calibrated transmission drops below 10%. The corrected spectra are in very good agreement with each other [cf. Fig. 2(e)]. The dominant remaining difference is visible at 40 nm

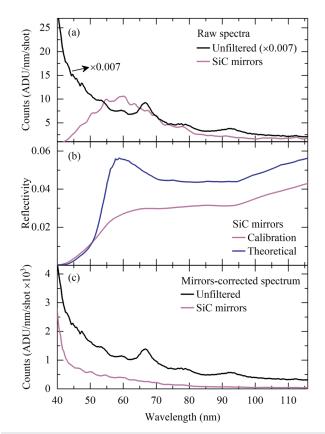
wavelength and can be attributed to the third-order contribution of the main emission feature at 13.5 nm that here only impacts the unfiltered spectrum and the Si filtered spectrum (the Zr-filtered spectrum is shown up to 18 nm where the transmission drops below 10%). The Al-filtered spectrum is free of this third-order diffraction feature and will be used for this wavelength range.

# 2. 40-115 nm wavelength range

For the investigation of the 40–115 nm wavelength range, we use the SiC mirrors. In Fig. 3(a), the spectrum obtained using the SiC mirrors is presented. In the same figure, a scaled unfiltered spectrum is also presented for comparison. The peak in the unfiltered spectrum in the 65–70 nm range can be attributed to the fifth diffraction order of the dominant 13.5 nm emission feature. The spectral intensities in the SiC mirror measurements are between two and three orders of magnitude lower than the unfiltered spectrum.

The SiC mirrors were sent to PTB for calibration in order to measure its total reflection efficiency. The resulting calibration is compared to the theoretical response curve in Fig. 3(b). The difference can be attributed partially to contamination but also to scattering due to roughness.

The LPP spectrum is then corrected with the reflectivity calibration data from PTB, the results of which are shown in Fig. 3(c).



**FIG. 3.** (a) Raw tin LPP emission spectra using the SiC mirrors and no filter. The unfiltered spectrum is multiplied by  $\times 0.007$  for better visibility. (b) SiC mirror reflectivity curves: one calibrated by PTB and one from theory (see main text). (c) Unfiltered spectrum and spectrum corrected for the SiC mirror reflectivity.

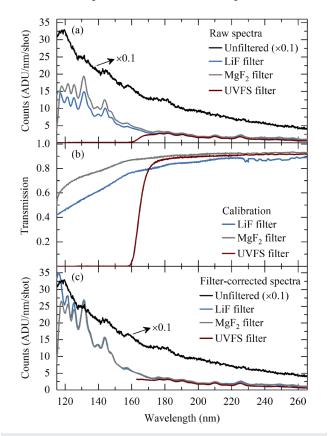
The unfiltered and SiC filtered spectra show significant differences, highlighting the important contribution from higher orders to the spectrum and emphasizing the need for suppression of higher orders using filters as is done here.

# 3. 115-265.5 nm wavelength range

To investigate the 115–265.5 nm wavelength range, we have recorded spectra using (i) no filter and the filters (ii) LiF, (iii) MgF<sub>2</sub>, and (iv) UVFS. The spectra are shown in Fig. 4(a). The spectrum with the LiF filter extends smoothly below 115 nm, but the spectrum recorded using the MgF<sub>2</sub> filter exhibits a steep decrease. The UVFS filter has the longest cutoff wavelength at 165 nm. All filters transmit at wavelengths above 265.5 nm, which is the limit of the measurement range set by the spectrometer.

In Fig. 4(b), the calibrated transmission efficiency curves of the three filters used for this wavelength region are presented. Since the upper limit of the wavelength axis of our recorded spectra is  $\sim$ 265.5 nm, a combination of two of the filters (either LiF or MgF<sub>2</sub> with UVFS) in the 115–265.5 nm range will fully suppress all higher-order contributions.

We present the filter-corrected spectra in Fig. 4(c). The three filter-corrected spectra are generally in good agreement with each other. The most significant difference, occurring below 120 nm, is



**FIG. 4.** (a) Raw emission spectra from a tin LPP using the LiF,  $MgF_2$ , and UVFS filter and no filter. The unfiltered spectrum is multiplied by ×0.1 for better visibility. (b) Filter transmission curves for the various filters. (c) Spectra corrected for the respective filter transmission functions.

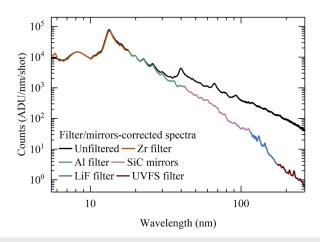


FIG. 5. Concatenated spectra from tin LPP using the various filters, corrected for the respective transmission functions (see main text). The chosen range for each spectrum is free of any higher diffraction orders. The unfiltered spectrum is also shown for comparison.

related to the accuracy of the onset of the transmission of the  $MgF_2$  filter and the precision of the relative wavelength calibration of the experiments and calibration. The comparison between the unfiltered spectrum and the filter-corrected spectra highlights the prominent contribution from high diffraction orders. The apparent intensity, i.e., counts, of the unfiltered spectrum is more than an order of magnitude stronger than the true signal, thus emphasizing the need to use filters.

In Fig. 5, we present the full spectrum in the 5.5–265.5 nm wavelength range obtained from concatenating the filtered spectra using only their respective ranges free of any higher diffraction orders. The individual y-axis values are shown to accurately "connect" at the respective overlap regions. We note that no free fit factors have been used to obtain this match. Instead, it is the accurate calibration of the filter transmissions that enables this good agreement. As seen before, strong contributions from higher diffraction orders are visible. In particular, the odd multiples of the main 13.5 nm emission feature stand out, starting from the third diffraction order.

#### **B.** Grating diffraction efficiency

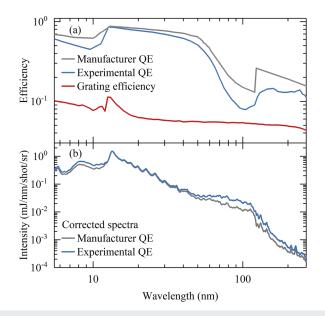
The first-order diffraction efficiency of the grating is shown in Fig. 6(a), as obtained from calibration at PTB. The feature that stands out is the "kink" near 12 nm that originates from the Si L-edge absorption in the Si<sub>3</sub>N<sub>4</sub> material present in the transmission grating.<sup>52</sup>

#### C. CCD response

The CCD camera response is a product of three components: the gain, quantum yield (QY), and quantum efficiency (QE).<sup>60</sup> The gain relates the ADU to the generated electrons and has the units of  $ADU/e^-$ . For the camera that is used in this experiment, the camera gain is specified by the manufacturer<sup>58</sup> as 0.83 ADU/ $e^-$ .

The QY is defined as the number of electrons generated per detected photon and is proportional to the energy of the photon. A typical assumption in the EUV and VUV wavelength ranges<sup>59,61</sup> is

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**FIG. 6.** (a) Grating efficiency for the first diffraction order and QE of the CCD camera, comparing manufacturer QE<sup>58</sup> or experimental QE<sup>59</sup> data (see main text). (b) Concatenated spectra (cf. Fig. 5) after correcting for the diffraction efficiency of the grating and the CCD response using either manufacturer or experimental QE data and solid angle.

that a photon energy of 3.66 eV, which corresponds to the indirect bandgap of Si, is needed to generate an electron. A detected photon of energy *E* would thus generate E/(3.66 eV) electrons. As pointed out also by Heymes *et al.*,<sup>61</sup> this assumption breaks down in the optical range where QY will instead converge to a value of 1. In the here studied wavelength range, however, the simple 1/3.66  $e^-/eV$  rule is in good agreement with a more detailed treatment.<sup>59,60</sup> Correcting for QY enables converting the number of electrons to the number of detected photons or to the amount of detected energy in units of eV with a proportionality constant of 3.66. Hence, the QY for the wavelength range explored in this work can be written in units of  $e^-/eV$  or  $e^-/mJ$  as QY =  $1/3.66e^-/eV = 1.71 \times 10^{15}e^-/mJ$ .

The QE is defined as the ratio of the number of detected photons to the number of photons arriving on the detector surface. Hence, it is also equal to the ratio of detected to incident energy. In Fig. 6(a), we show two such quantum efficiency curves. The first is obtained from the manufacturer of the CCD used in our experiments.<sup>58</sup> We note however that the calibration provided by the manufacturer depends, in part, on simulations and not experiments.<sup>62</sup> According to their simulations, the sharp edge around 120 nm originates from thin film interference, assuming a sharp interface between the assumed SiO<sub>2</sub> layer and the active Si CCD surface. In reality, the boundary is expected to be less sharp due to intermixing. As a result, the QE curve is expected to have a smoother shape. In search of experimental support for our QE calibration, we employ the recent results.<sup>59</sup> Further experimental QE studies are found in previous works.<sup>62-64</sup> Comparing the two QE curves in Fig. 6(a), we note that there is a striking difference near 120 nm where a sharp, steep edge is visible in the QE from the manufacturer, which is not supported (either in amplitude or shape) by recent experimental

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TABLE II. Energy emitted toward the spectrometer, i.e., under a 60° angle (cf. Fig. 1)	
in the various wavelength ranges using manufacturer QE data (cf. Fig. 6).	

Wavelength range (nm)	Corresponding filter	Energy (mJ shot <sup>-1</sup> sr <sup>-1</sup> )	(%) of total energy
5.5-17.5	Zr	7.1	54.7
$(13.5 \text{ nm} \pm 1\%^{a})$	(Zr)	(0.4)	(3.1)
17.5-42.5	Al	4.2	32.5
42.5-115	SiC	1.5	11.4
115-175.5	LiF	0.2	1.2
175.5-265.5	UVFS	0.03	0.2
Total energy	13.0		

 $^{\rm a}The$  value for the energy emitted in the 2%-wavelength bandwidth centered around 13.5 nm is impacted on by the limited resolution of the spectrometer (0.8 nm at 13.5 nm).

work.<sup>59</sup> The differences between the available QE curves may be due to dissimilarities in manufacturing processes or, for instance, due to possible aging effects. Considering the significant differences, the overall uncertainty in our final spectrum is expected to be dominated by the QE curve.

As the final step, the concatenated spectra of Fig. 5 are corrected for the camera response (gain, QY, and QE) together with the solid angle of the spectrometer  $(37 \times 10^{-11} \text{ sr})$ , and the resulting corrected full-range spectrum is shown in Fig. 6(b). Integral energies emitted in the various wavelength ranges, following the filters used, are presented in Table II. The final corrections, using either QE curve, produce a "knee" near 120 nm wavelength that is not visible in the concatenated data of Fig. 5, which may point at a discrepancy between the true QE and the available QE curves.

Further corrections for the source size (possibly weakly wavelength-dependent) and for the precise time dependence of the transient emission are required to interpret the obtained intensity in terms of spectral radiance. These steps are left as future work but may be expected to have only limited impact on the overall shape of the emission spectrum, as shown in Fig. 6(b). Nevertheless, the obtained spectrum enables diagnosing the energy distribution of the LPP that is useful for optimizing the LPP based EUV sources.

# **IV. CONCLUSIONS**

We present a fully calibrated spectrum in the 5.5-265.5 nm range from a microdroplet-tin Nd:YAG-laser-produced plasma. The spectrum obtained using a transmission grating spectrometer is the result of a careful calibration of a series of filters enabling measurements free of any higher diffraction orders. Specifically, we use Zr, Si, and Al foil filters and bulk LiF, MgF<sub>2</sub>, and UVFS filters. A further filter using four SiC mirrors is used to record the otherwise inaccessible 40-100 nm region. The photon energy in this particular wavelength range is significant and provides input for further studies on the impact of EUV-induced-plasma in the EUV source vessel. The fully corrected and concatenated spectra are shown to accurately match in their respective overlap regions, demonstrating the accuracy of the calibration procedure. The dominant remaining uncertainty stems from the correction for quantum efficiency. Our calibration enables the optimization of current and future sources of EUV light for nanolithography by providing metrology for

minimizing the emission of unwanted wavelength bands that may limit imaging contrast or even impact machine uptime.

# SUPPLEMENTARY MATERIAL

See the supplementary material for the data presented in Figs. 5 and 6(b).

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## AUTHOR DECLARATIONS

#### **Conflict of Interest**

The authors have no conflicts to disclose.

#### DATA AVAILABILITY

The data that support the findings of this study are available from the corresponding author upon reasonable request. The particular data that support the findings of this study as presented in Figs. 5 and 6(b) are available within the article and its supplementary material.

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